# Comparison among Two Analytical Methods of Multi-Criteria Decision Making for Appropriate Spinning Condition Selection 

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#### Abstract

This paper makes an attempt to evaluate final ranking of the alternatives proposed by two different approaches of multi-criteria decision making (MCDM) in detecting the suitable spinning process variables for spun yarn intended to be used in knitting process. Performances of three variables in a draw frame were evaluated on the basis of seven quality parameters of the forty eight rotor yarns using technique for order preference by similarity to ideal solutions (TOPSIS) and vlseKriterijumska optimizacija i kompromisno resenje (VIKOR). Both methods are based on an aggregating function illustrating closeness to the ideal. Linear normalization and vector normalization are used in VIKOR and TOPSIS respectively to eliminate the units of criterion function. Difference in normalization technique affected final rankings as they introduced two different alternatives as the best. It means that, selecting appropriate MCDM method to rank feasible alternatives and accepting proposed yarn sample or process condition is related to the economical advantages and efficiency of the spinning and knitting processes.


Key words: Multi-criteria decision making - TOPSIS approach • VIKOR method • Draw frame • Rotor spun yarn - Weft knitted fabric

## INTRODUCTION

Yarn production process is accompanied by drafting of staple fibers assemblies from beginning to the end. In a drafting arrangement, break draft, roller setting, production speed and top arm pressure are some important variables that affect drafting quality [1]. From 1950 many researchers have focused on perception of relationship between these parameters and their effects on yarn structure and its properties [2, 3].

Studies show that, relationship between abovementioned variables and yarn characteristics is very deep and complex [4-6]. Therefore, selecting suitable processing condition among available alternatives is a difficult task and better outcomes about the desired final product properties will be achieved if the priorities of the spinner are taken into account [7].

In recent years, multi-criteria decision making (MCDM) has been employed extensively in various scientific disciplines [8]. Suitable nozzles in a rotor spin-box have been selected by ELECTRE outranking
method [7]. Organic fibers have been ranked by MCDM approach [9]. The technological value of the cotton fibers is determined by a hybrid method of MCDM [10]. This method was used to chose cotton fibers and lay-down in a blow-room [11].

MCDM is a branch of operations research (OR). This technique treats with solving problems while a finite number of decision criteria and alternatives are present. TOPSIS and VIKOR are widely used methods of MCDM. Since, there is not published literature that focuses on comparing selection of alternatives using these methods in the field of textile, this study makes an attempt to use them in reaching acceptable solution in order to select the appropriate draw frame parameters that results spun yarn with the best quality parameters to use in weft knitting process and to compare their final rankings.

A Brief Overview of TOPSIS: Multi-criteria decision making is a complex process consists of one managerial level and one engineering level. Such kind of the problem is expressed in decision matrix format.

[^0]|  | $C_{1}$ | $C_{2}$ | $\ldots$ | $C n$ |
| :---: | :---: | :---: | :---: | :---: |
| $A_{1}$ | $x_{11}$ | $x_{12}$ | $\ldots$ | $x_{1 n}$ |
| $A_{2}$ | $x_{21}$ | $x_{22}$ | $\ldots$ | $x_{2 n}$ |
| $A m$ | $x_{m 1}$ | $x_{m 2}$ | $\ldots$ | $x_{m n}$ |

where; $A_{1}, A_{2}, . ., A m$ are available alternatives. Decision makers have to choose among these alternatives. $C_{1}, C_{3}$ $\ldots, C_{n}$ are criteria with which alternative performance are measured, $x_{i j}$ is the rating of alternative $A i$ with respect to the criterion $C_{j}$ [12].

Hwang and Yoon (1981) developed TOPSIS for solving a MCDM problem. In this method, the selected alternative should have the shortest distance from the positive ideal solution and the farthest distance from the negative ideal solution [12, 13]. Below steps show the procedure of TOPSIS in details [12].

- Calculating normalized decision matrix ( $r_{i j}$ values)

$$
\begin{equation*}
r_{i j}=f_{i j} / \sqrt{\sum_{j=1}^{J} f_{i j}^{2}}, j=1, \ldots,, J \quad i=1, \ldots n \tag{1}
\end{equation*}
$$

- Calculating weighted normalized decision matrix ( $v_{i j}$ value)

$$
\begin{equation*}
v_{i j}=\omega_{i} r_{i j}, \quad j=1, \ldots J, \quad i=1, \ldots n, \tag{2}
\end{equation*}
$$

where $\omega_{i}$ is the weight of the $i^{\text {ih }}$ attribute or criterion and $\sum_{i=1}^{n} \omega_{i}=1$

- Determining the positive and negative ideal solutions
$A^{+}=\left\{v_{1}{ }^{+}, \ldots . . v_{n}{ }^{+}\right\}=\left\{\left(\max _{j} v_{i j} \mid i \in I\right),\left(\min _{j} v_{i j} \mid i \in J\right)\right\}$
$A^{-}=\left\{v_{1}^{-}, \ldots . . v_{n}{ }^{-}\right\}=\left\{\left(\min _{j} v_{i j} \mid i \in I\right),\left(\max _{j} v_{i j} \mid i \in J\right)\right\}$

In these equations $I$ is associated with benefit criteria and $J$ is associated with cost criteria:

- Calculating separation measure using the $n$ dimensional Euclidean distance

$$
\begin{align*}
& {D_{j}^{+}}_{j}=\sqrt{\sum_{i=1}^{n}\left(v_{i j}-v_{i}^{+}\right)^{2}} \quad j=1, \ldots, J .  \tag{5}\\
& D_{j}^{-}=\sqrt{\sum_{i=1}^{n}\left(v_{i j}-v_{i}^{-}\right)^{2}} \quad j=1, \ldots, J \tag{6}
\end{align*}
$$

- Calculate the relative closeness to the ideal solution of the alternative $A_{j}$ with respect to $A^{+}$.
$C C^{*}{ }_{j}=D_{j}^{-} /\left(D_{j}^{+}+D_{j}^{-}\right), \quad j=1, \ldots, J$.
For $D_{j}^{-} \geq 0$ and $D_{j}^{+} \geq 0, C C^{*} j \in[0,1]$
- Ranking the preference order.

A Brief Overview of VIKOR: In the engineering studies after generating the alternatives, MCDM methods are used to propose a solution to the decision-maker [14]. Opricovic and Tzeng presented VIKOR method for multi-criteria optimization of complex systems [15, 16]. VIKOR is borrowed from Serbian and means multi-criteria optimization and compromise solution [17]. The compromise ranking-list, the compromise solution and the weight stability intervals for priorities stability of the compromise solution got with the initial weights are determined by VIKOR [14].

Each alternative is assessed according to each criterion function. The compromise ranking could be conducted by comparing the measure of closeness to the ideal solution $f^{*}$. The compromise solution $f^{c}$ is defined as a solution with the shortest distance to the ideal solution. The multi-criteria measure is developed from the $L_{p}$-metric used as an aggregating function in a compromise programming technique. Denote alternatives as $a_{\mathrm{⿺}}, a_{2}, \ldots$, $a_{j}$. For alternative $a_{j}$ the rating of the $i^{\text {th }}$ aspect shown by $f_{i j}$, i.e. $f_{i j}$ is the measure of the $i^{\text {th }}$ criterion function. Following form of the $L_{p}$-metric is used to develop the VIKOR.

$$
\begin{equation*}
L_{P, j}=\left\{\sum_{i=1}^{n}\left[w_{i}\left(f_{i}^{*}-f_{i j}\right) /\left(f_{i}^{*}-f_{i}^{-}\right)\right]^{p}\right\}^{1 / p} 1 \leq p \leq \infty \quad j=1,2, . \tag{8}
\end{equation*}
$$

$L_{1, j}\left(S_{j}\right.$ in Equation 9) and $L_{*, j}\left(R_{j}\right.$ in Equation 10) are employed to formulate ranking value. The solution proposed by $\min _{j} S_{j}$ is accompanied by a maximum group utility (majority rule). Beside, the solution achieved by $\min _{j} R_{j}$ is with a minimum individual regret of the opponent. $F^{c}$ is a solution with the shortest distance from the ideal $F^{*}$. Compromise means agreement developed by mutual concessions by $\Delta f_{1}=f_{1}^{*}-f_{1}^{c}$ and $\Delta f_{2}=f_{2}^{*}-f_{2}^{c}$. Ranking alternatives by VIKOR is conducted in five steps.

- Determining the best $f_{i}^{*}$ and the worst $f_{i}$ values of all criterion functions by decision makers. If the $i^{\text {th }}$ function shows a benefit: $f_{i}^{*}=\max _{j} f_{i j}$ and $f_{i}^{-}=\min _{j} f_{i j}$
- The values of $S_{j}$ and $R_{j}, j=1,2, \ldots, J$ are calculated by the following relations.

$$
\begin{align*}
& S_{j}=\sum_{i=1}^{n} w_{i}\left(f_{i}^{*}-f_{i j}\right) /\left(f_{i}^{*}-f_{i}^{-}\right)  \tag{9}\\
& R_{j}=\max _{i} w_{i}\left[\left(f_{i}^{*}-f_{i j}\right) /\left(f_{i}^{*}-f_{i}^{-}\right)\right] \tag{10}
\end{align*}
$$

- The values of $Q_{j}, j=1,2, \ldots, J$ are computed.
$Q_{j}=V\left(S_{J}-S_{J}{ }^{*}\right) /\left(S_{J}{ }^{-}-S_{J}{ }^{*}\right)+(1-v)\left(R_{j}-R_{j}^{*}\right) /\left(R_{j}^{-}-R_{j}^{*}\right)$
where; $S^{*}=\min _{j} S_{j}, S^{-}=\max _{j} S_{j}, R^{*}=\min _{j} R_{j}, R^{-}=\max _{j} R_{j}$
The solutions calculated by $S^{*}$ and $R^{*}$ are with a maximum group utility and minimum individual regret of the opponent respectively. $v$ is the weight of the strategy of the majority of criteria.
- Sorting the values of $S, R, Q$ in decreasing order to rank the alternatives. The results are illustrated in three ranking lists.
- The alternative $\left(a^{\prime}\right)$ is considered the best by the measure $(Q)$ if the below two conditions are satisfied.
- Acceptable benefit; $Q\left(a^{\prime \prime}\right)-Q\left(a^{\prime}\right) \geq 1 /(1 /(J-1)$
where $a^{\prime \prime}$ is the alternative with the second position in the ranking list by $Q$
- For acceptable stability in decision making, alternative $a^{\prime}$ must be the best ranked by $S$ or / and $R$

If one condition is not satisfied, a set of compromise solutions is proposed.

- Alternatives $a^{\prime}$ and $a^{\prime \prime}$ if only condition 2 is not satisfied.
- Alternatives $a^{\prime}$ and $a^{\prime \prime}$ and $a^{M}$ if condition 1 is not satisfied. $a^{M}$ is determined by the relation $Q\left(a^{M}\right)-$ $Q\left(a^{\prime}\right) \leqslant 1 /(J-1)$ for maximum M (the positions of these alternatives are in closeness) $[14,18]$.


## MATERIALS AND METHODS

The average fiber length, micronaire and maturity index were $27 \mathrm{~mm}, 3.6$ and 0.85 respectively. Cotton fibers were furnished as a second draw frame sliver with linear density of 5.2ktex to produce 30 Ne yarn on a Rieter RU04 rotor spinning machine with $900 \mathrm{~T} / \mathrm{m}$. The opening roller was designed at a speed of 8200 rpm . The 35 mm diameter rotor worked at a speed of 75000 rpm . There were three main parameters in draw frame including delivery speed of $550,650,700$ and $750 \mathrm{~m} / \mathrm{min}$, distance between back and middle rolls of $8,10,12$ and 14 mm and break draft of 1.14 , 1.41 and 1.70 . Specifications of the yarn samples have been shown in Table 1.

A test specimen of 500 mm was elongated at an extension rate of $500 \mathrm{~mm} / \mathrm{min}$ to examine load-elongation characteristics using Uster Tensorapid3. The unevenness

Table 1: Specifications of cotton rotor yarn samples

|  | Variables |  |  |  | Variables |  |  |  | Variables |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Alt | DBBMR | DS | BD | Alt | DBBMR | DPS | BD | Alt | DBBMR | DS | BD |
| A1 | 8 | 750 | 1.70 | A17 | 10 | 550 | 1.41 | A33 | 10 | 750 | 1.70 |
| A2 | 14 | 750 | 1.41 | A18 | 10 | 750 | 1.14 | A34 | 8 | 550 | 1.41 |
| A3 | 14 | 550 | 1.41 | A19 | 12 | 650 | 1.70 | A35 | 8 | 650 | 1.14 |
| A4 | 14 | 550 | 1.70 | A20 | 10 | 650 | 1.14 | A36 | 10 | 550 | 1.70 |
| A5 | 12 | 550 | 1.70 | A21 | 8 | 550 | 1.70 | A37 | 12 | 750 | 1.70 |
| A6 | 8 | 700 | 1.70 | A22 | 10 | 700 | 1.41 | A38 | 14 | 650 | 1.41 |
| A7 | 12 | 650 | 1.14 | A23 | 8 | 700 | 1.41 | A39 | 14 | 650 | 1.70 |
| A8 | 8 | 650 | 1.70 | A24 | 10 | 700 | 1.70 | A40 | 10 | 650 | 1.70 |
| A9 | 12 | 700 | 1.41 | A25 | 14 | 750 | 1.14 | A41 | 12 | 650 | 1.41 |
| A10 | 10 | 700 | 1.14 | A26 | 8 | 700 | 1.14 | A42 | 14 | 700 | 1.41 |
| A11 | 12 | 750 | 1.41 | A27 | 14 | 700 | 1.41 | A43 | 14 | 700 | 1.14 |
| A12 | 14 | 750 | 1.70 | A28 | 8 | 650 | 1.41 | A44 | 10 | 650 | 1.41 |
| A13 | 10 | 750 | 1.41 | A29 | 14 | 550 | 1.14 | A45 | 8 | 550 | 1.14 |
| A14 | 12 | 750 | 1.14 | A30 | 14 | 650 | 1.14 | A46 | 10 | 550 | 1.14 |
| A15 | 12 | 700 | 1.70 | A31 | 12 | 550 | 1.14 | A47 | 12 | 550 | 1.41 |
| A16 | 8 | 750 | 1.41 | A32 | 12 | 700 | 1.14 | A48 | 10 | 550 | 1.14 |

Table 2: Quality parameters of the yarns (Performance values of the alternatives)

|  | Y.T | B.E | CV\% | T.P | T.P | Y.N | Y.H |  | Y.T | B.E | CV\% | T.P | T.P | Y.N | Y.H |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Alt | $\mathrm{X}_{6}{ }^{+}$ | $\mathrm{X}_{7}{ }^{+}$ | $\mathrm{X}_{1}{ }^{\text {- }}$ | $\mathrm{X}_{2}{ }^{-}$ | $\mathrm{X}_{3}{ }^{-}$ | $\mathrm{X}_{4}{ }^{-}$ | $\mathrm{X}_{5}^{-}$ | Alt | $\mathrm{X}_{6}{ }^{+}$ | $\mathrm{X}_{7}^{+}$ | $\mathrm{X}_{1}^{-}$ | $\mathrm{X}_{2}{ }^{-}$ | $\mathrm{X}_{3}{ }^{\text {+ }}$ | $\mathrm{X}_{4}{ }^{\text {- }}$ | $\mathrm{X}_{5}{ }^{-}$ |
| A1 | 15.06 | 6.80 | 14.56 | 25.20 | 62.40 | 31.20 | 6.54 | 25 | A25 | 14.98 | 6.59 | 14.94 | 36.40 | 66.20 | 35.80 |
| A2 | 14.90 | 6.65 | 14.65 | 28.80 | 56.00 | 35.80 | 5.19 | 26 | A26 | 15.39 | 6.73 | 14.85 | 34.80 | 71.60 | 49.60 |
| A3 | 13.00 | 6.24 | 15.13 | 41.80 | 81.20 | 49.40 | 5.79 | 27 | A27 | 14.54 | 6.42 | 14.54 | 25.40 | 53.60 | 21.60 |
| A4 | 15.25 | 6.68 | 14.78 | 37.20 | 43.80 | 19.60 | 6.48 | 28 | A28 | 14.59 | 6.43 | 14.51 | 35.00 | 50.00 | 28.60 |
| A5 | 14.70 | 6.67 | 14.65 | 25.20 | 54.20 | 24.20 | 4.99 | 29 | A29 | 12.77 | 6.67 | 14.57 | 28.00 | 73.50 | 36.00 |
| A6 | 14.28 | 6.80 | 14.38 | 28.20 | 46.80 | 23.00 | 5.09 | 30 | A30 | 15.46 | 6.83 | 15.05 | 35.50 | 92.00 | 71.00 |
| A7 | 13.42 | 6.45 | 14.93 | 41.40 | 70.20 | 33.40 | 5.62 | 31 | A31 | 13.97 | 6.65 | 15.10 | 45.50 | 75.00 | 39.50 |
| A8 | 14.10 | 6.67 | 14.68 | 35.80 | 35.80 | 31.80 | 5.33 | 32 | A32 | 13.62 | 6.50 | 15.30 | 43.50 | 82.00 | 26.00 |
| A9 | 12.63 | 6.27 | 15.11 | 38.20 | 38.20 | 49.20 | 5.13 | 33 | A33 | 13.34 | 6.58 | 14.92 | 38.50 | 67.50 | 28.50 |
| A10 | 13.00 | 6.70 | 14.58 | 30.20 | 30.20 | 27.40 | 5.75 | 34 | A34 | 14.05 | 6.72 | 14.78 | 26.50 | 73.50 | 31.50 |
| A11 | 12.89 | 6.42 | 14.73 | 34.40 | 63.80 | 31.60 | 5.25 | 35 | A35 | 14.58 | 6.78 | 15.61 | 34.50 | 57.00 | 33.00 |
| A12 | 14.02 | 6.71 | 15.01 | 34.80 | 53.20 | 34.00 | 6.41 | 36 | A36 | 14.11 | 6.61 | 14.70 | 32.50 | 60.00 | 34.00 |
| A13 | 13.36 | 6.17 | 14.68 | 32.60 | 63.20 | 30.80 | 5.70 | 37 | A37 | 14.46 | 6.73 | 15.11 | 43.50 | 74.50 | 49.00 |
| A14 | 14.80 | 6.28 | 14.92 | 51.60 | 72.20 | 38.20 | 5.75 | 38 | A38 | 13.38 | 6.43 | 14.65 | 33.00 | 60.00 | 30.90 |
| A15 | 14.22 | 6.35 | 14.71 | 29.40 | 59.60 | 25.20 | 5.73 | 39 | A39 | 13.33 | 6.51 | 15.31 | 55.00 | 98.50 | 64.50 |
| A16 | 14.64 | 6.46 | 14.21 | 20.80 | 40.60 | 22.40 | 5.58 | 40 | A40 | 14.65 | 6.43 | 14.71 | 42.00 | 75.00 | 39.50 |
| A17 | 13.99 | 6.28 | 15.09 | 34.40 | 82.20 | 65.60 | 5.68 | 41 | A41 | 15.13 | 6.76 | 14.81 | 30.00 | 71.16 | 26.00 |
| A18 | 15.20 | 6.63 | 14.48 | 16.20 | 50.40 | 29.00 | 5.39 | 42 | A42 | 13.22 | 6.47 | 14.97 | 34.50 | 73.00 | 46.00 |
| A19 | 13.85 | 6.40 | 14.66 | 36.40 | 60.40 | 33.20 | 5.71 | 43 | A43 | 12.85 | 6.61 | 14.74 | 32.50 | 64.50 | 36.00 |
| A20 | 13.85 | 6.41 | 14.35 | 23.20 | 46.60 | 28.80 | 5.40 | 44 | A44 | 13.96 | 6.63 | 14.58 | 24.00 | 56.00 | 27.00 |
| A21 | 13.98 | 6.39 | 14.70 | 30.80 | 64.20 | 34.80 | 5.12 | 45 | A45 | 14.07 | 6.57 | 14.42 | 19.00 | 51.50 | 19.50 |
| A22 | 15.21 | 6.56 | 14.24 | 26.20 | 48.20 | 26.80 | 6.58 | 46 | A46 | 14.98 | 6.72 | 14.45 | 24.50 | 59.00 | 31.00 |
| A23 | 14.25 | 6.33 | 15.18 | 40.20 | 94.40 | 71.80 | 5.74 | 47 | A47 | 14.13 | 6.40 | 14.47 | 24.50 | 54.50 | 28.50 |
| A24 | 14.70 | 6.53 | 14.66 | 26.20 | 56.20 | 30.40 | 5.20 | 48 | A48 | 13.23 | 6.37 | 14.45 | 22.50 | 50.50 | 23.50 |

Y.T: yarn tenacity ( $\mathrm{cN} /$ tex) B.E: breaking elongation (\%) CV: coefficient of mass variation (\%) T.P: thin places ( $-50 \%$ ) T.P: thick places ( $+50 \%$ ) Y.N: yarn neps (+280\%) Y.H: yarn hairiness (H)
and imperfections of 5 samples for each group were measured with an Uster Tester 4 with a test speed of $400 \mathrm{~m} / \mathrm{min}$ for 2.5 min . The hairiness of 10 samples with length of 100 mm was measured with Premier Tester 7000 . Table 2 shows the results of the experiments.

## RESULTS

Performing TOPSIS Approach: A one-way ANOVA test ( $5 \%$ significance level) was applied to determine the effects of considered parameters on yarn quality parameters. Average values of the yarn quality parameters were grouped according to the Duncan Multiple Range Test.

The mechanical and physical properties of a yarn running into a circular knitting machine are important technological parameter that affects machine efficiency. Higher tenacity and elongation at break of the yarn and lower friction between yarn and machine surfaces such as needle are useful to reduce yarn breakage. Hairiness is a factor that affects friction between needle and yarn. Increase in hairiness and wrapper fibers, produces more friction between the yarn and metal surface and increase
yarn bending flexural rigidity. Increase in friction leads to an increase in yarn tension and breakage [19-22]. However, mechanical properties of a yarn are a function of yarn imperfections and unevenness. The more the imperfections and unevenness are the more yarn breakages occur [23].

If a ranking between these properties is needed the most important one to increase machine efficiency is assumed to be yarn hairiness followed by unevenness, thick places, neps, thin places, tenacity and elongation. Tenacity and elongation are shown by positive sign. Also, hairiness, coefficient of mass variation (CV\%) and imperfections are shown by negative sign in the investigation.

Relative importance of the effective factors on machine efficiency was picked up based on the 24 experts, opinions that were proficient in weft knitting industry. Table 3 shows results of the discussion about importance of the rotor yarn properties and relative importance of each criterion.

The decision matrix obtained from average values of yarn quality parameters has been shown in Table 2. At the next step normalized decision matrix was calculated using

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Table 3: Intensity of the effect of yarn properties on weft knitting machine efficiency

| Company | Y.T | B.E | Y.H | CV | TP | TP | Y.N |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Relative or mean importance $\left(\mathrm{RI}_{\mathrm{j}}\right)$ | 7.375 | 3.875 | 9.875 | 9.750 | 9.750 | 4.625 | 9.250 |
| Weight of each criterion $\left(R I_{j} / \sum_{j=1}^{j=n} R I_{j}\right)$ | 0.085 | 0.075 | 0.191 | 0.189 | 0.189 | 0.089 | 0.179 |


|  | Y.T | B.E | Y.H | CV | TP | TP | Y.N |  | Y.T | B.E | Y.H | CV | TP | TP | Y.N |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Alt | $\mathrm{X}_{6}^{+-----}$ | $\mathrm{X}_{7}^{+}---$ | $\mathrm{X}_{1}^{------}$ | $\mathrm{X}_{2}^{------}$ | $\mathrm{X}_{3}^{------}$ | $\begin{aligned} & ------1 \\ & \mathrm{X}_{4}^{-} \end{aligned}$ | $\begin{aligned} & ------1 \\ & X_{5}^{-} \end{aligned}$ | Alt | $\mathrm{X}_{6}^{+----}$ | $\mathrm{X}_{7}^{+}----$ | $\begin{aligned} & ------\quad \\ & X_{1}^{-} \end{aligned}$ | $\mathrm{X}_{2}^{------}$ | $\mathrm{X}_{3}^{------}$ | $\mathrm{X}_{4}^{------}$ | $\mathrm{X}_{5}^{-----}$ |
| A1 | 0.150 | 0.150 | 0.142 | 0.107 | 0.140 | 0.120 | 0.167 | 25 | A25 | 0.149 | 0.145 | 0.146 | 0.155 | 0.149 | 0.138 |
| A2 | 0.149 | 0.146 | 0.143 | 0.123 | 0.126 | 0.138 | 0.132 | 26 | A26 | 0.154 | 0.148 | 0.145 | 0.149 | 0.161 | 0.192 |
| A3 | 0.130 | 0.137 | 0.147 | 0.179 | 0.183 | 0.191 | 0.147 | 27 | A27 | 0.145 | 0.141 | 0.142 | 0.108 | 0.121 | 0.083 |
| A4 | 0.152 | 0.147 | 0.144 | 0.159 | 0.098 | 0.075 | 0.165 | 28 | A28 | 0.145 | 0.141 | 0.141 | 0.149 | 0.112 | 0.110 |
| A5 | 0.147 | 0.147 | 0.143 | 0.107 | 0.122 | 0.093 | 0.127 | 29 | A29 | 0.127 | 0.147 | 0.142 | 0.119 | 0.166 | 0.139 |
| A6 | 0.142 | 0.149 | 0.140 | 0.120 | 0.105 | 0.089 | 0.129 | 30 | A30 | 0.154 | 0.150 | 0.147 | 0.152 | 0.207 | 0.275 |
| A7 | 0.134 | 0.142 | 0.145 | 0.177 | 0.158 | 0.129 | 0.143 | 31 | A31 | 0.139 | 0.146 | 0.147 | 0.194 | 0.169 | 0.153 |
| A8 | 0.141 | 0.147 | 0.143 | 0.153 | 0.080 | 0.123 | 0.136 | 32 | A32 | 0.136 | 0.143 | 0.149 | 0.186 | 0.185 | 0.100 |
| A9 | 0.126 | 0.138 | 0.147 | 0.163 | 0.086 | 0.190 | 0.130 | 33 | A33 | 0.133 | 0.145 | 0.145 | 0.164 | 0.152 | 0.110 |
| A10 | 0.130 | 0.147 | 0.142 | 0.129 | 0.068 | 0.106 | 0.146 | 34 | A34 | 0.140 | 0.148 | 0.144 | 0.113 | 0.166 | 0.122 |
| A11 | 0.128 | 0.141 | 0.143 | 0.147 | 0.144 | 0.122 | 0.134 | 35 | A35 | 0.145 | 0.149 | 0.152 | 0.147 | 0.128 | 0.127 |
| A12 | 0.140 | 0.147 | 0.146 | 0.149 | 0.120 | 0.131 | 0.163 | 36 | A36 | 0.141 | 0.145 | 0.143 | 0.139 | 0.135 | 0.131 |
| A13 | 0.133 | 0.136 | 0.143 | 0.139 | 0.142 | 0.119 | 0.145 | 37 | A37 | 0.144 | 0.148 | 0.147 | 0.186 | 0.168 | 0.189 |
| A14 | 0.148 | 0.138 | 0.145 | 0.221 | 0.163 | 0.148 | 0.146 | 38 | A38 | 0.133 | 0.141 | 0.143 | 0.141 | 0.135 | 0.119 |
| A15 | 0.142 | 0.140 | 0.143 | 0.125 | 0.134 | 0.097 | 0.146 | 39 | A39 | 0.133 | 0.143 | 0.149 | 0.235 | 0.222 | 0.250 |
| A16 | 0.146 | 0.142 | 0.138 | 0.089 | 0.091 | 0.086 | 0.142 | 40 | A40 | 0.146 | 0.141 | 0.143 | 0.179 | 0.169 | 0.153 |
| A17 | 0.139 | 0.138 | 0.147 | 0.147 | 0.185 | 0.254 | 0.145 | 41 | A41 | 0.151 | 0.149 | 0.144 | 0.128 | 0.160 | 0.100 |
| A18 | 0.152 | 0.146 | 0.141 | 0.069 | 0.113 | 0.112 | 0.137 | 42 | A42 | 0.132 | 0.142 | 0.146 | 0.147 | 0.164 | 0.178 |
| A19 | 0.138 | 0.141 | 0.143 | 0.155 | 0.136 | 0.128 | 0.145 | 43 | A43 | 0.128 | 0.145 | 0.144 | 0.139 | 0.145 | 0.139 |
| A20 | 0.138 | 0.141 | 0.140 | 0.099 | 0.105 | 0.111 | 0.137 | 44 | A44 | 0.139 | 0.146 | 0.142 | 0.102 | 0.126 | 0.104 |
| A21 | 0.139 | 0.140 | 0.143 | 0.131 | 0.145 | 0.134 | 0.130 | 45 | A45 | 0.140 | 0.144 | 0.140 | 0.081 | 0.116 | 0.075 |
| A22 | 0.152 | 0.144 | 0.139 | 0.112 | 0.108 | 0.103 | 0.168 | 46 | A46 | 0.149 | 0.148 | 0.141 | 0.104 | 0.133 | 0.120 |
| A23 | 0.142 | 0.139 | 0.148 | 0.172 | 0.213 | 0.278 | 0.146 | 47 | A47 | 0.141 | 0.141 | 0.141 | 0.104 | 0.123 | 0.110 |
| A24 | 0.147 | 0.143 | 0.143 | 0.112 | 0.126 | 0.117 | 0.132 | 48 | A48 | 0.132 | 0.140 | 0.141 | 0.096 | 0.114 | 0.091 |

data shown in Table 2. Normalized decision matrix has been shown in Table 4. Considering the different importance of each criterion and calculating vector of the criteria, the weighted normalized decision matrix was constructed using Equation 2. Calculated matrix has been shown in Table 5.

At the fifth step of the TOPSIS method, the positive and the negative ideal solution $\left(A^{+}\right)$and $\left(A^{-}\right)$were determined. Values of $\left(A^{+}\right)$and $\left(A^{-}\right)$have been shown below as two vectors.

After identifying $\left(A^{+}\right)$and $\left(A^{-}\right)$the separation of each alternative from the ideal solution are given. Distance of each alternative from the ideal solution can be seen in Table 7. Relative closeness of the alternatives $\left(C C_{j}\right)$ to the ideal solution $\left(A_{j}\right)$ were defined by the last equation with respect to $A^{+}$. Results of calculation are shown in Table 8.

Performing VIKOR Approach: Relative importance of the criteria considered from one to ten and decision matrix were the same for both algorithms. Considering the different importance of each criterion and calculating vector of the criteria, the normalized decision matrix was constructed using linear normalization technique for VIKOR method. Calculated matrix has been shown in Table 9.

The first step in decision making using VIKOR approach is obtaining the best and the worst values for each criterion functions. At the second step the values of $S_{j}$ and $R_{j}, j=1,2, \ldots, J$ are calculated based on the Equations 9,10 and weight of each criterion when ${ }_{[R 5]} v=0.50$. As mentioned above, $v$ is the weight of the strategy of the majority of criteria. Here we can use $v=0.50$ for final ranking. Table 10 shows the values of $Q_{j}, S_{j}$ and $R_{j}$ when $v=0.50_{[R 6]}$.

Table 5: The weighted normalized decision matrix

|  | Y.T | B.E | Y.H | CV | TP | TP |  | Y.N | Y.T | B.E | Y.H | CV | TP | TP | Y.N |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Alt | $\mathrm{X}_{6}^{+}$ | $\mathrm{X}_{7}^{+}$ | $\mathrm{X}_{1}{ }^{-}$ | $\mathrm{X}_{2}{ }^{-}$ | $\mathrm{X}_{3}{ }^{-}$ | $\mathrm{X}_{4}{ }^{-}$ | Alt | $\mathrm{X}_{5}{ }^{-}$ | $\mathrm{X}_{6}{ }^{+}$ | $\mathrm{X}_{7}^{+}$ | $\mathrm{X}_{1}{ }^{-}$ | $\mathrm{X}_{2}{ }^{-}$ | $\mathrm{X}_{3}{ }^{-}$ | $\mathrm{X}_{4}{ }^{-}$ | $\mathrm{X}_{5}{ }^{-}$ |
| 1 | 0.012 | 0.011 | 0.026 | 0.009 | 0.026 | 0.021 | 25 | 0.032 | 25 | 0.012 | 0.010 | 0.027 | 0.014 | 0.028 | 0.024 |
| 2 | 0.012 | 0.011 | 0.027 | 0.011 | 0.023 | 0.024 | 26 | 0.025 | 26 | 0.013 | 0.011 | 0.027 | 0.013 | 0.030 | 0.034 |
| 3 | 0.011 | 0.010 | 0.028 | 0.016 | 0.034 | 0.034 | 27 | 0.028 | 27 | 0.012 | 0.010 | 0.026 | 0.009 | 0.022 | 0.015 |
| 4 | 0.012 | 0.011 | 0.027 | 0.014 | 0.018 | 0.013 | 28 | 0.031 | 28 | 0.012 | 0.010 | 0.026 | 0.013 | 0.021 | 0.019 |
| 5 | $0.012$ | 0.011 | 0.027 | 0.009 | 0.023 | 0.016 | 29 | 0.024 | 29 | 0.010 | 0.011 | 0.026 | 0.010 | 0.031 | 0.025 |
| 6 | 0.012 | 0.011 | 0.026 | 0.010 | 0.020 | 0.016 | 30 | 0.024 | 30 | 0.013 | 0.011 | 0.027 | 0.013 | 0.039 | 0.049 |
| 7 | $0.011$ | $0.010$ | $0.027$ | $0.015$ | $0.030$ | $0.023$ | 31 | $0.027$ | 31 | $0.011$ | $0.011$ | $0.027$ | $0.017$ | $0.032$ | 0.027 |
| 8 | $0.011$ | 0.011 | 0.027 | 0.013 | 0.015 | 0.022 | 32 | 0.026 | 32 | 0.011 | 0.010 | 0.028 | 0.016 | 0.035 | 0.018 |
| 9 | 0.010 | 0.010 | 0.027 | 0.014 | 0.016 | 0.034 | 33 | 0.025 | 33 | 0.011 | 0.010 | 0.027 | 0.014 | 0.028 | 0.019 |
| 10 | $0.011$ | $0.011$ | $0.026$ | $0.011$ | $0.012$ | $0.019$ | 34 | 0.028 | 34 | 0.011 | 0.011 | 0.027 | 0.010 | 0.031 | 0.021 |
| 11 | $0.010$ | 0.010 | 0.027 | 0.013 | 0.027 | 0.022 | 35 | 0.025 | 35 | 0.012 | 0.011 | 0.028 | 0.013 | 0.024 | 0.022 |
| 12 | 0.011 | 0.011 | 0.027 | 0.013 | 0.022 | 0.023 | 36 | 0.031 | 36 | 0.011 | 0.010 | 0.027 | 0.012 | 0.025 | 0.023 |
| 13 | $0.011$ | $0.010$ | 0.027 | $0.012$ | 0.027 | 0.021 | 37 | 0.027 | 37 | 0.012 | 0.011 | 0.027 | 0.016 | 0.031 | 0.034 |
| 14 | 0.012 | 0.010 | 0.027 | 0.019 | 0.030 | 0.026 | 38 | 0.028 | 38 | 0.011 | 0.010 | 0.027 | 0.012 | 0.025 | 0.021 |
| 15 | 0.012 | 0.010 | 0.027 | 0.011 | 0.025 | 0.017 | 39 | 0.028 | 39 | 0.011 | 0.010 | 0.028 | 0.021 | 0.042 | 0.044 |
| 16 | 0.012 | 0.010 | 0.026 | 0.008 | 0.017 | 0.015 | 40 | 0.027 | 40 | 0.012 | 0.010 | 0.027 | 0.016 | 0.032 | 0.027 |
| 17 | 0.011 | 0.010 | 0.027 | 0.013 | 0.035 | 0.045 | 41 | 0.027 | 41 | 0.012 | 0.011 | 0.027 | 0.011 | 0.030 | 0.018 |
| 18 | 0.012 | 0.011 | 0.026 | 0.006 | 0.021 | 0.020 | 42 | 0.026 | 42 | 0.011 | 0.010 | 0.027 | 0.013 | 0.031 | 0.032 |
| 19 | 0.011 | 0.010 | 0.027 | 0.014 | 0.025 | 0.023 | 43 | 0.027 | 43 | 0.010 | 0.010 | 0.027 | 0.012 | 0.027 | 0.025 |
| 20 | 0.011 | 0.010 | 0.026 | 0.008 | 0.019 | 0.020 | 44 | 0.026 | 44 | 0.011 | 0.011 | 0.026 | 0.009 | 0.023 | 0.018 |
| 21 | 0.011 | 0.010 | 0.027 | 0.011 | 0.0274 | 0.024 | 45 | 0.025 | 45 | 0.011 | 0.010 | 0.026 | 0.007 | 0.022 | 0.013 |
| 22 | 0.012 | 0.010 | 0.026 | 0.010 | 0.020 | 0.018 | 46 | 0.032 | 46 | 0.012 | 0.011 | 0.026 | 0.009 | 0.025 | 0.021 |
| 23 | 0.01 | 0.010 | 0.028 | 0.015 | 0.040 | 0.050 | 47 | 0.028 | 47 | 0.012 | 0.010 | 0.026 | 0.009 | 0.023 | 0.019 |
| 24 | 0.012 | 0.010 | 0.027 | 0.010 | 0.024 | 0.021 | 48 | 0.025 | 48 | 0.011 | 0.010 | 0.026 | 0.008 | 0.021 | 0.016 |

Table 6: Values of positive and negative ideal solution

|  | CV | T.P | T.P | Y.N | Y.H | T | B.E |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ideal solution | $\mathrm{X}_{1}$ | $\mathrm{X}_{2}{ }^{-}$ | $\mathrm{X}_{3}{ }^{-}$ | $\mathrm{X}_{4}{ }^{\text {- }}$ | $\mathrm{X}_{5}{ }^{\text {- }}$ | $\mathrm{X}_{6}^{+}$ | $\mathrm{X}_{7}^{+}$ |
| $A^{+}$ | 0.026 | 0.006 | 0.012 | 0.013 | 0.024 | 0.013 | 0.011 |
| $A^{-}$ | 0.028 | 0.021 | 0.042 | 0.050 | 0.032 | 0.010 | 0.010 |

Table 7: Distance of each alternative from the positive and negative ideal solution

| Alt | $\left(D^{+}\right)$ | $\left(D^{-}\right)$ | Alt | $\left(D^{+}\right)$ | $\left(D^{-}\right)$ | Alt | $\left(D^{+}\right)$ | $\left(D^{-}\right)$ | Alt | $\left(D^{+}\right)$ | $\left(D^{-}\right)$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| A1 | 0.020 | 0.034 | A13 | 0.020 | 0.034 | A25 | 0.022 | 0.030 | A37 | 0.031 | 0.021 |
| A2 | 0.018 | 0.033 | A14 | 0.028 | 0.026 | A26 | 0.031 | 0.021 | A38 | 0.019 | 0.035 |
| A3 | 0.033 | 0.018 | A15 | 0.017 | 0.038 | A27 | 0.016 | 0.042 | A39 | 0.046 | 0.008 |
| A4 | 0.015 | 0.044 | A16 | 0.010 | 0.045 | A28 | 0.015 | 0.038 | A40 | 0.028 | 0.025 |
| A5 | 0.014 | 0.041 | A17 | 0.041 | 0.012 | A29 | 0.024 | 0.030 | A41 | 0.020 | 0.036 |
| A6 | 0.012 | 0.043 | A18 | 0.014 | 0.040 | A30 | 0.047 | 0.009 | A42 | 0.029 | 0.024 |
| A7 | 0.024 | 0.030 | A19 | 0.020 | 0.033 | A31 | 0.028 | 0.026 | A43 | 0.022 | 0.031 |
| A8 | 0.015 | 0.040 | A20 | 0.013 | 0.040 | A32 | 0.028 | 0.033 | A44 | 0.015 | 0.039 |
| A9 | 0.025 | 0.032 | A21 | 0.021 | 0.032 | A33 | 0.023 | 0.034 | A45 | 0.013 | 0.044 |
| A10 | 0.013 | 0.044 | A22 | 0.015 | 0.040 | A34 | 0.023 | 0.032 | A46 | 0.017 | 0.036 |
| A11 | 0.021 | 0.033 | A23 | 0.048 | 0.008 | A35 | 0.019 | 0.034 | A47 | 0.016 | 0.038 |
| A12 | 0.019 | 0.034 | A24 | 0.016 | 0.037 | A36 | 0.019 | 0.033 | A48 | 0.014 | 0.042 |

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Table 8: Relative closeness coefficient of each alternative to the ideal solution

| Alt | ( $C C$ j) | Alt | $\left(C C_{j}\right)$ | Alte | $\left(C C_{j}\right)$ | Alt | $\left(C C_{j}\right)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A1 | 0.635 | A13 | 0.628 | A25 | 0.577 | A37 | 0.398 |
| A2 | 0.645 | A14 | 0.490 | A26 | 0.408 | A38 | 0.648 |
| A3 | 0.356 | A15 | 0.692 | A27 | 0.726 | A39 | 0.144 |
| A4 | 0.749 | A16 | 0.815 | A28 | 0.716 | A40 | 0.474 |
| A5 | 0.745 | A17 | 0.233 | A29 | 0.552 | A41 | 0.637 |
| A6 | 0.777 | A18 | 0.746 | A30 | 0.155 | A42 | 0.452 |
| A7 | 0.557 | A19 | 0.617 | A31 | 0.484 | A43 | 0.585 |
| A8 | 0.732 | A20 | 0.747 | A32 | 0.543 | A44 | 0.717 |
| A9 | 0.562 | A21 | 0.606 | A33 | 0.596 | A45 | 0.774 |
| A10 | 0.773 | A22 | 0.727 | A34 | 0.588 | A46 | 0.676 |
| A11 | 0.619 | A23 | 0.137 | A35 | 0.647 | A47 | 0.708 |
| A12 | 0.634 | A24 | 0.692 | A36 | 0.630 | A48 | 0.750 |

Table 9: The normalized decision matrix

|  | Y.T | B.E | CV | T.P | T.P | Y.N | Y.H |  | Y.T | B.E | CV | T.P | T.P | Y.N | Y.H |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Alt | ------ | ------ | X1- | X2- | X3- | ----- | X5- | Alt | ------ | ------ | X1- | ------ | ----- | X4- | X5- |
| A1 | 0.974 | $0.996$ | $0.975$ | $0.642$ | $0.483$ | $0.625$ | $0.755$ | A25 | 0.968 | $0.965$ | $0.950$ | 0.445 | 0.456 | 0.544 | 0.923 |
| A2 | 0.964 | 0.973 | 0.969 | 0.562 | 0.539 | 0.544 | 0.951 | A26 | 0.996 | 0.985 | 0.957 | 0.465 | 0.421 | 0.393 | $0.745^{*}$ |
| A3 | 0.840 | 0.913 | 0.939 | 0.387 | 0.371 | 0.394 | 0.853 | A27 | 0.940 | 0.939 | 0.977 | 0.637 | 0.563 | 0.902 | 0.754 |
| A4 | 0.986 | 0.979 | 0.961 | 0.435 | 0.689 | 0.994 | 0.762 | A28 | 0.943 | 0.941 | 0.979 | 0.462 | 0.604 | 0.681 | $1.000^{* *}$ |
| A5 | $0.950$ | $0.977$ | $0.969$ | $0.642$ | $0.557$ | $0.805$ | $0.989$ | A29 | 0.826 | $0.977$ | $0.975$ | $0.578$ | 0.410 | 0.541 | 0.948 |
| A6 | 0.923 | 0.995 | 0.988 | 0.574 | 0.645 | 0.847 | 0.970 | A30 | $1.000^{*}$ | $1.000^{*}$ | 0.944 | 0.456 | 0.328 | 0.274 | 0.749 |
| A7 | 0.868 | 0.944 | 0.951 | 0.391 | 0.430 | 0.583 | 0.879 | A31 | 0.903 | 0.973 | 0.941 | 0.356 | 0.402 | 0.493 | 0.955 |
| A8 | 0.912 | 0.977 | 0.967 | $0.452$ | $0.843$ | 0.613 | 0.926 | A32 | 0.880 | 0.952 | 0.928 | 0.372 | 0.368 | 0.750 | 0.753 |
| A9 | $0.816^{* *}$ | 0.918 | 0.940 | 0.424 | 0.790 | 0.396 | 0.962 | A33 | 0.862 | 0.964 | 0.952 | 0.420 | 0.447 | 0.684 | 0.754 |
| A10 | 0.840 | 0.980 | 0.974 | 0.536 | $1.000^{* *}$ | 0.711 | 0.859 | A34 | 0.908 | 0.983 | 0.961 | 0.611 | 0.410 | 0.619 | 0.880 |
| A11 | 0.833 | 0.939 | 0.964 | 0.470 | 0.473 | 0.617 | 0.940 | A35 | 0.943 | 0.992 | 0.910* | 0.469 | 0.529 | 0.590 | 0.948 |
| A12 | 0.907 | 0.982 | 0.946 | 0.465 | 0.567 | 0.573 | 0.770 | A36 | 0.912 | 0.967 | 0.966 | 0.498 | 0.503 | 0.573 | 0.968 |
| A13 | 0.864 | $0.903^{* *}$ | 0.968 | 0.496 | 0.477 | 0.633 | 0.866 | A37 | 0.935 | 0.985 | 0.940 | 0.372 | 0.405 | 0.397 | 0.932 |
| A14 | 0.957 | 0.920 | 0.952 | 0.313 | 0.418 | 0.510 | 0.859 | A38 | 0.866 | 0.941 | 0.970 | 0.490 | 0.503 | 0.631 | 0.946 |
| A15 | 0.920 | 0.929 | 0.966 | 0.551 | 0.506 | 0.773 | 0.862 | A39 | 0.862 | 0.953 | 0.928 | $0.294^{*}$ | $0.306^{*}$ | 0.302 | 0.908 |
| A16 | 0.947 | 0.945 | $1.000^{* *}$ | 0.778 | 0.743 | 0.870 | 0.885 | A40 | 0.947 | 0.941 | 0.965 | 0.385 | 0.402 | 0.493 | 0.757 |
| A17 | 0.904 | 0.919 | 0.941 | 0.470 | 0.367 | 0.297 | 0.869 | A41 | 0.978 | 0.990 | 0.959 | 0.540 | 0.424 | 0.750 | 0.932 |
| A18 | 0.983 | 0.970 | 0.981 | $1.000^{* *}$ | 0.599 | 0.672 | 0.916 | A42 | 0.855 | 0.948 | 0.949 | 0.469 | 0.413 | 0.423 | 0.950 |
| A19 | 0.895 | 0.936 | 0.969 | 0.445 | 0.500 | 0.587 | 0.865 | A43 | 0.831 | 0.967 | 0.963 | 0.498 | 0.468 | 0.541 | 0.953 |
| A20 | 0.896 | 0.939 | 0.990 | 0.698 | 0.648 | 0.677 | 0.914 | A44 | 0.902 | 0.970 | 0.974 | 0.675 | 0.539 | 0.722 | 0.964 |
| A21 | 0.904 | 0.935 | 0.966 | 0.525 | 0.470 | 0.560 | 0.964 | A45 | 0.910 | 0.961 | 0.985 | 0.852 | 0.586 | $1.000^{* *}$ | 0.896 |
| A22 | 0.984 | 0.960 | 0.997 | 0.618 | 0.626 | 0.727 | 0.750 | A46 | 0.968 | 0.983 | 0.983 | 0.661 | 0.511 | 0.629 | 0.919 |
| A23 | 0.921 | 0.926 | 0.936 | 0.402 | 0.319 | $0.271{ }^{*}$ | 0.860 | A47 | 0.913 | 0.936 | 0.982 | 0.661 | 0.554 | 0.684 | 0.872 |
| A24 | 0.951 | 0.955 | 0.969 | 0.618 | 0.537 | 0.641 | 0.950 | A48 | 0.855 | 0.932 | 0.983 | 0.720 | 0.598 | 0.829 | 0.862 |

** Shows the worst value and * shows the best value for the criterion

Comparing Final Ranking of the Alternatives and Discussion: The results of TOPSIS analysis are summarized in Table 8 and Figure 2. Based on the $C C_{j}$ values ranking of the preference order of all alternatives in descending order is as below. According to the last step, the best alternative is selected as sample No. 16 with
closeness coefficient of 0.815 and the worst alternative is sample No. 23 with closeness coefficient of 0.137 . According to the final ranking, yarn sample spun at processing condition in which distance between back and middle rolls is 8 mm , delivery speed is $750 \mathrm{~m} / \mathrm{min}$ and break draft is 1.41 has the best performance.


Fig. 2: Ranking the preference order (descending) of all alternatives


Fig. 3: Ranking the preference order of more important alternatives after sensitivity analysis


The worst alternative
Fig. 4: Ranking the preference order (descending) of all alternatives


Fig. 5: Ranking the preference order of 10 important alternatives after sensitivity analysis

Values of the relative importance are expressed by decision makers. Since, this parameter is not certainly stable, it is important to know the effect of deviation in these values on final ranking. To test this influence, sensitivity analysis is conducted. The idea of sensitivity analysis is decreasing and increasing all the weights of the criteria ( $5 \%, 10 \%, 15 \%, 20 \%$ ) according to the Equation 12 and repeating TOPSIS approach with new values.
$W_{i}^{n e w}=W_{i} \pm \alpha W_{i}$ and $\alpha=\{0.05,0.1,0.15,0.2\}$
The main condition in Table 8 expresses the original result of the case study. Figure 3 illustrates the graphical representation for only 9 more important alternatives of these results that were in prior final ranking due to limitation. According to the Figure, it was concluded that, ranking of 4 more important alternatives (A16, A6, A45, A10) is approximately as same as previous main ranking. Alternatives show a straight or nearly straight line trend and their position in new ranking is stable while considered weight for each yarn property changes.

The results of VIKOR analysis are summarized in Table 10 and Figure 4. Based on the values of $S, R, Q$ ranking of the preference order of all alternatives in descending order is as below (descending order).

According to the last step, the best alternative for weft knitting machine is selected as sample No. 30 with $Q_{j}$, $S_{j}$ and $R_{j}$ of $0,0.058,0.031$ respectively and the worst alternative is sample No. 3 with $Q_{j}, S_{j}$ and $R_{j}$ of $0.830,0.478$ and 0.774 . On the other hand, according to the final ranking, yarn sample spun at processing condition in which distance between back and middle rolls was 14 mm , delivery speed was $650 \mathrm{~m} / \mathrm{min}$ and break draft is 1.14 had
the best performance. It means it is expected that if this yarn sample is used in a circular knitting machine to produce fabric, the knittability is higher while there be less yarn breakage as well.

Sensitivity analysis is conducted by changing values of $v$ or the weight of the strategy of the majority of criteria. The idea of sensitivity analysis is decreasing and increasing $v$ value from zero to one by step of 0.1 . The main condition in Table 10 expresses the original result of the case study. Figure 5 illustrates the graphical representation for these alternatives due to space limitation. According to the sensitivity analysis results, ranking of more important alternatives (A30, A26, A1, A12) is approximately as same as previous main ranking. Alternatives show a straight or nearly straight line trend and their position in new ranking is stable while considered $v$ for each yarn property changes. ${ }_{[\text {[R8] }}$

Findings of the research confirm the effect of difference in TOPSIS and VIKOR procedure steps on final ranking of the alternatives. Aggregation function and normalization methods for eliminating the units of criterion function used by TOPSIS and VIKOR techniques are different. Linear normalization employed by VIKOR is independent of the evaluation unit of a criterion. Normalized values proposed by vector normalization in TOPSIS are different when different evaluation unit is used in a particular criterion.

The relative importance of all criteria and a balance between total and individual satisfaction are considered when an aggregating function is represented by VIKOR. This case in not taken into account when aggregating function is represented by TOPSIS. Final ranking proposed by VIKOR is acceptable only for the given set of alternatives [8]. Also, VIKOR approach determines the

| Alt | $Q_{j}$ | $S_{j}$ | $R_{j}$ | Alt | $Q_{j}$ | $S_{j}$ | $R_{j}$ | Alt | $Q_{j}$ | $S_{j}$ | $R_{j}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A1 | 0.154 | 0.229 | 0.061 | A17 | 0.365 | 0.414 | 0.159 | A33 | 0.302 | 0.354 | 0.134 |
| A2 | 0.368 | 0.422 | $0.153$ | A18 | $0.391$ | $0.474$ | $0.127$ | A34 | 0.295 | 0.376 | $0.100$ |
| A3 | 0.830 | 0.478 | 0.774 | A19 | 0.395 | 0.480 | 0.125 | A35 | $0.301$ | 0.340 | 0.150 |
| A4 | 0.663 | 0.324 | 0.707 | A20 | 0.497 | 0.610 | 0.126 | A36 | 0.422 | 0.481 | $0.166$ |
| A5 | 0.450 | 0.502 | 0.181 | A21 | 0.469 | 0.543 | 0.163 | A37 | 0.270 | 0.311 | $0.138$ |
| A6 | 0.453 | 0.518 | 0.167 | A22 | 0.274 | 0.359 | 0.087 | A38 | 0.484 | 0.573 | 0.149 |
| A7 | 0.381 | 0.461 | 0.128 | A23 | 0.304 | 0.348 | 0.145 | A39 | 0.314 | 0.370 | 0.135 |
| A8 | $0.445$ | 0.526 | 0.146 | A24 | 0.417 | 0.486 | $0.152$ | A40 | 0.241 | $0.293$ | $0.116$ |
| A9 | $0.599$ | $0.693$ | $0.179$ | A25 | $0.305$ | $0.360$ | $0.132$ | A41 | $0.296$ | $0.343$ | $0.138$ |
| $\mathrm{A} 10$ | $0.539$ | 0.608 | 0.189 | A26 | $0.073$ | 0.142 | 0.044 | A42 | $0.429$ | $0.501$ | $0.152$ |
| A11 | $0.504$ | $0.586$ | $0.163$ | A27 | $0.353$ | $0.432$ | $0.119$ | A43 | $0.464$ | $0.534$ | $0.165$ |
| A12 | $0.234$ | $0.306$ | $0.091$ | A28 | $0.513$ | $0.576$ | $0.189$ | A44 | $0.465$ | $0.537$ | $0.163$ |
| A13 | $0.520$ | $0.583$ | $0.191$ | A29 | $0.455$ | $0.519$ | $0.170$ | A45 | $0.459$ | $0.573$ | $0.112$ |
| A14 | $0.343$ | $0.386$ | $0.158$ | $\mathrm{A} 30$ | $0.000$ | $0.058$ | $0.031$ | A46 | $0.335$ | $0.401$ | $0.129$ |
| A15 | $0.420$ | $0.501$ | $0.139$ | A31 | $0.346$ | $0.392$ | $0.156$ | A47 | $0.434$ | $0.530$ | $0.125$ |
| A16 | 0.479 | 0.593 | 0.119 | A32 | 0.261 | 0.318 | 0.116 | A48 | 0.509 | 0.625 | 0.141 |

weight stability intervals [14]. Researcher believed that, selecting appropriate MCDM algorithm to rank feasible alternatives and accepting proposed sample and condition is related to economical advantages and knitting machine performance while producing yarn and knitted fabric samples.

## CONCLUSION

The purpose of the study is to compare performances of TOPSIS and VIKOR approaches in obtaining suitable spinning condition for rotor spun yarn. Qualitative parameters of the forty eight different yarn samples were assessed. Then, these characteristics were evaluated with the purpose of using the yarn in weft knitted fabric and to increase machine efficiency. Relative steps of the TOPSIS and VIKOR algorithms were executed for available data and finally the ranking of the alternatives were performed. Based on the final ranking represented by TOPSIS yarn sample spun when distance between back and middle rolls is 8 mm , delivery speed is $750 \mathrm{~m} / \mathrm{min}$ and break draft is 1.41 has the best performance among available alternatives. VIKOR method showed that, yarn sample spun at processing condition in which distance between back and middle rolls is 14 mm , delivery speed is $650 \mathrm{~m} / \mathrm{min}$ and break draft is 1.14 is the most preferred one among the alternatives for knitting process. Difference between proposed rankings can be due to normalization method applied in these algorithms. Selection of the best alternative is depended to the economical advantages in yarn and fabric production and also, ease of spinning preparation machines setting.

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