

Maximum Power Point Tracking Technique

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Abstract: Non-renewable sources of energy have been under scrutiny during the last decade. Exhaustive use of such resources has forced mankind to go in other resources that will last long. Harnessing solar energy has been the best solution to meet the growing needs. A battery less solar harvesting circuit that meets low power applications is discussed here. The main intention is to harvest abundant solar energy under non-stationary light conditions by maximum-power-point-tracking method. Fractional Open Circuit Voltage (FVoc) method is proposed in the present solar power module. This method is the most economical power tracking method out of all the present methods. This method is based upon the fact that the pv array voltage corresponding to the maximum power exhibits a linear relationship with the array open circuit voltage at different irradiation and temperature levels. Sampling a portion of the array voltage is achieved through a Sample and Hold amplifier. The most special feature of the proposed method is that the circuit does not utilize any expensive micro controller or a digital signal processor and hence this is most suited for micro applications.

Key words: Maximum Power Point Tracking • Fractional Open Circuit Voltage (Fvoc) • Solar Array • S&H Amplifier • Sampling time • Trigger Outputs

INTRODUCTION

Constant and excessive use of non conventional energy sources has led to its replenishment at a much faster rate than expected. This has forced us to think of other alternate sources to meet the enormously growing power requirements. The only solution to meet the current requirement is none other than opting for renewable energy sources. The most economical and simplest to implement of all those is none other than the infinite energy from the sun that is said to last for several thousand years to come [1].

Renewable energy sources are known to be much cleaner and produce energy without the harmful effects of pollution unlike their conventional counterparts [2].

Photovoltaic (PV) systems, present the desirable features of being modular and easily deployable on rooftops, close to the consumers. Also photovoltaic offers an environmentally friendly source of electricity [1], of which the fuel is sunshine, a renewable energy. This method of power generation, however, has been relatively costly compared to other methods. The success of a PV

application depends on whether the power electronics device can extract sufficiently high power from the PV arrays to keep overall output power per unit cost low.

The maximum power point tracking (MPPT) [5] of the PV output for all sunshine conditions, therefore, becomes a key control in the device operation for successful PV applications.

The MPPT control [5] is challenging, because the solar irradiance and temperature that determines the amount of solar energy into the PV array may change all the time and the current voltage characteristic of PV arrays is highly nonlinear. The optimal operation of a PV system is important. A real time MPPT technique is required to obtain maximum power from a PV system.

Tracking Techniques: Solar irradiance is not constant and varies gradually throughout the day. Irrespective of the change in available solar energy, a constant, maximum output is to be acquired. This can be achieved by 2 ways.

- Altering the position of the array mechanically.
- Through electronic tracking techniques.

The second method is analysed and discussed in the project, wherein, tracking the maximum power point (MPP) [3] and making the solar array to operate at the MPP constantly is achieved. MPPT is a fully electronic system that varies the electrical operating point of the modules so that the modules [2] are able to deliver maximum available power.

The components for the systems includes

- Solar Panel
- Triggering circuit to aid MPP Tracking
- PWM generator circuit
- An ac load

Structuring a PV Array: A PV array consists of several photovoltaic cells in series and parallel connections. Series connections are responsible for increasing the voltage of the module whereas the parallel connection is responsible for increasing the current in the array. Typically a solar cell can be modelled by a current source and an inverted diode connected in parallel to it. It has its own series and parallel resistance.

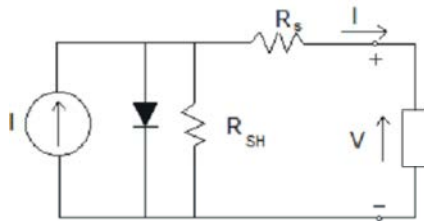


Fig. 1: Elementary model of a PV cell

Series resistance is due to hindrance in the path of flow of electrons from n to p junction and parallel resistance is due to the leakage current.

In this model [6] we consider a current source (I) along with a diode and series resistance (R_s). The shunt resistance (R_{sh}) in parallel is very high, has a negligible effect and can be neglected. The output current from the photovoltaic array is:

$$I = I_{SC} - I_d$$

$$I_d = I_0(e^{qV_d/KT} - 1)$$

where, I_0 is the reverse saturation current of the diode, q is the electron charge, V_d is the voltage across the diode, k is Boltzmann constant (1.38×10^{-19} J/K) and T is the junction temperature in Kelvin (K):

$$I = I_{SC} - I_0(e^{qV_d/KT} - 1)$$

Using suitable approximations,

$$I = I_{SC} - I_0(e^{q(V+IR_s)/nKT} - 1)$$

where, I is the photovoltaic cell current, V is the PV cell voltage, T is the temperature (in Kelvin) and n is the diode ideality factor. In order to model the solar panel accurately we can use two diode model [5] but in our project our scope of study is limited to the single diode model. Also, the shunt resistance is very high and can be neglected during the course of our study.

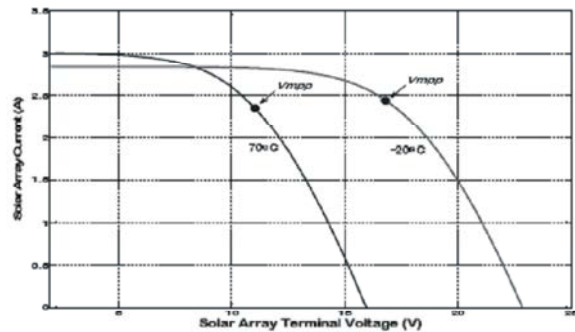


Fig. 2: Non-Linear V-I characteristics of a PV array

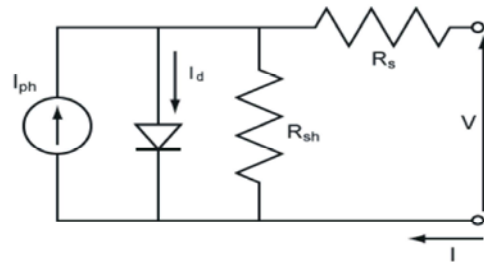


Fig. 3: Equivalence of a solar circuit

Fvoc Technique: The near linear relationship between V_{MPP} and V_{OC} [5] of the PV array, under varying irradiance and temperature levels, has given rise to the fractional V_{OC} method.

$$V_{MPP} = K_1 V_{OC}$$

where k_1 is a constant of proportionality [4]. Since k_1 is dependent on the characteristics of the PV array being used, it usually has to be computed beforehand by empirically determining V_{MPP} and V_{OC} for the specific PV array at different irradiance and temperature levels. The factor k_1 has been reported to be between 0.71 and 0.78 [2].

Once k_1 is known, V_{MPP} can be computed with V_{oc} measured periodically by momentarily shutting down the power converter. However, this incurs some disadvantages, including temporary loss of power. To prevent this, uses pilot cells [5] from which V_{oc} can be obtained. These pilot cells must be carefully chosen to closely represent the characteristics of the PV array.

The voltage generated by pn-junction diodes is approximately 75% of V_{oc} [4]. This eliminates the need for measuring V_{oc} and computing V_{MPP} . Once V_{MPP} has been approximated, a closed loop control on the array power converter can be used to asymptotically reach this desired voltage. This is only an approximation, the PV array technically never operates at the MPP. Depending on the application of the PV system, this can sometimes be adequate.

Even if fractional V_{oc} is not a true MPPT technique [6], it is very easy and cheap to implement as it does not necessarily require DSP or microcontroller control [3]. However, it points out that k_1 is no more valid in the presence of partial shading (which causes multiple local maxima) of the PV array and proposes sweeping the PV array voltage to update k . This obviously adds to the implementation complexity and incurs more power loss.

Low Power MPPT: The voltage based MPPT technique is based on the fact that the PV array voltage corresponding to the maximum power exhibits a linear dependence with respect to the array open circuit voltage for different irradiation and temperature levels [3], i.e.,

$$V_{mpp} = M_v \cdot V_{oc}$$

where,

V_{mpp} is the maximum power point voltage,
 V_{oc} is the open circuit voltage of the PV array
 M_v is the voltage factor.

The voltage factor has the value between 0.7-0.8 [4] depending upon the PV array characteristics.

To operate the PV panel at the MPP, the actual PV array voltage V_{pv} is compared with the reference voltage V_{ref} , which corresponds to the V_{mpp} . The error signal is then processed to make $V_{pv} = V_{ref}$. Normally, the panel is disconnected from the load momentarily to sample its open circuit voltage.

The fraction of the open circuit voltage corresponding to the V_{mpp} is measured and is kept in a hold circuit [7] to function as V_{ref} for the control loop. Even though the voltage based MPPT method is

classified as quasi seek method, but research has shown that this method has efficiency comparable to the P&O and IC [5] method under normal illumination conditions. This method is also considered to be the simplest and cost effective. Low-power systems for tracking the peak power point are presented. They exploit microcontroller and analog circuits to track MPP during light variations. The size of the adopted PV modules is greater than 20cm square, which is enough to provide tens of milli-watts and to perform an efficient power collection. In particular, supports different power sources and tries to eliminate the overhead in cost and power consumption caused by a microprocessor-based algorithm for MPPT.

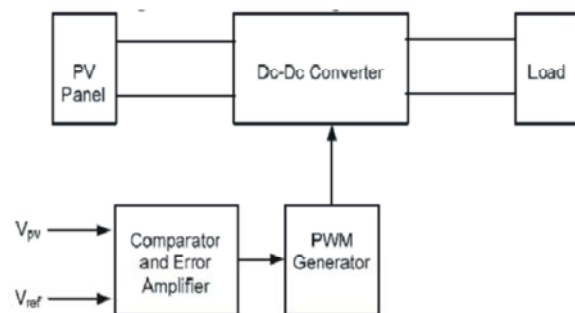


Fig. 4: MPPT Block Diagram

The harvesting unit is independent from the target system and it requires the presence of a rechargeable battery as secondary buffer to work when the primary buffer is empty. The adopted technique to estimate the position of the MPP relies on a light sensor (e.g., photodiode) and they associate this information to the solar-cell characteristic.

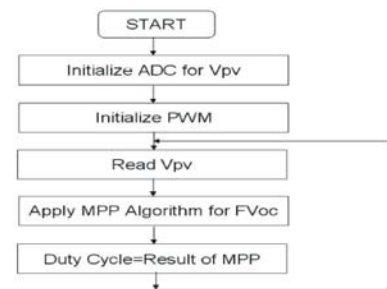


Fig. 5: MPPT Flow Diagram

Hardware Detailing: The basic circuit diagram for FVoc method [3] is indicated below. It consists of 2 major portions. They are listed below:

- Main harvester circuit with PV panel.
- Triggering circuit [3] with one astablemultivibrator and 2 monostablemultivibrator.

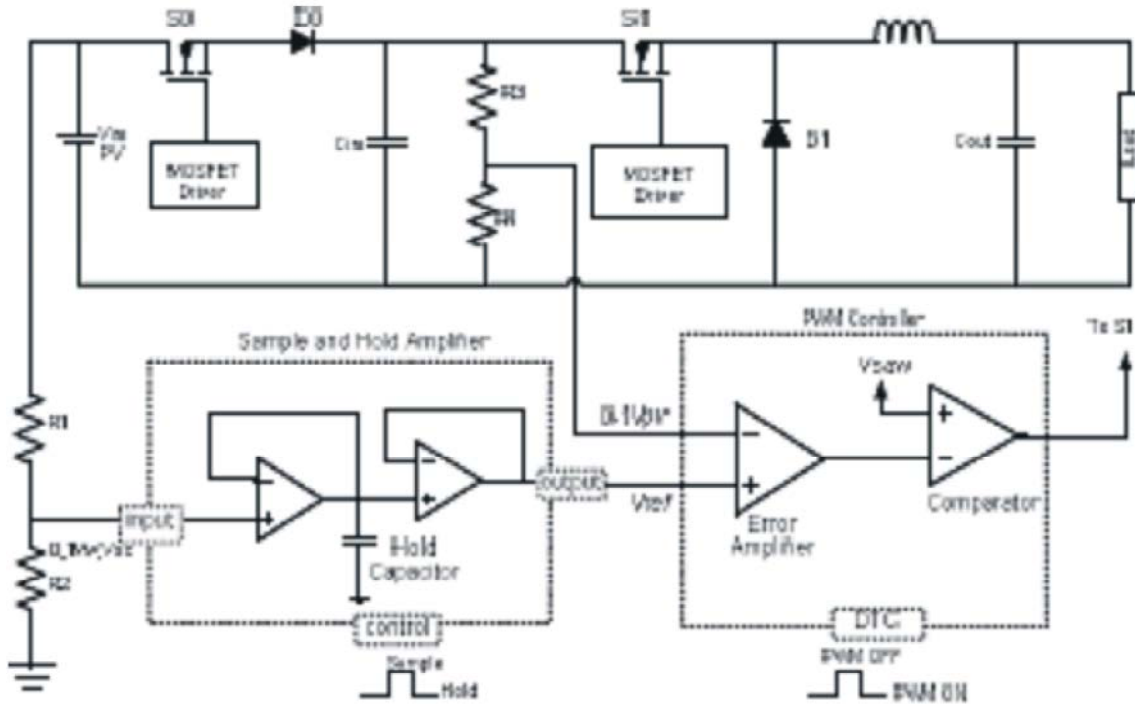


Fig. 6: FVoc Circuit Diagram

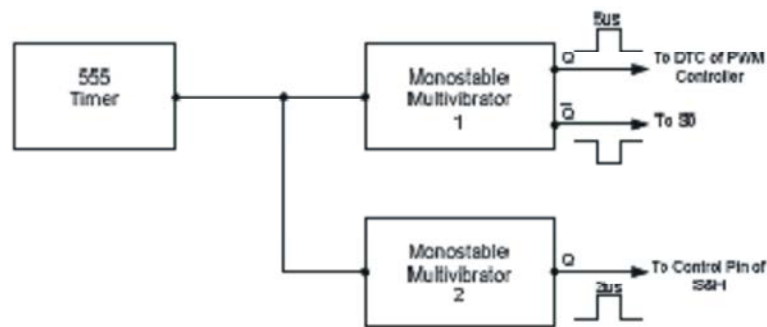


Fig. 7: Block diagram of the triggering circuit

The above figures show the circuit diagram of the proposed MPPT. S0 is the static switch used for disconnecting the PV array from the load for the sampling of the array voltage. D0 is the reverse blocking diode and S1 is the main switching

MOSFET. In the proposed MPPT the S&H [7] has a fast acquisition time.

The reason for choosing the S&H with fast acquisition time is to reduce the sampling time and, consequently, the power annulment period. The S&H also has a low droop rate to avoid the deviation of the PV operating point from the MPP during the sampling period, as discussed in the previous section. The sampling period

is chosen to be 100ms. The combination of short sampling period and low droop rate of the S&H obviates the need for using extended hold time S&H thereby decreasing the number of components in the proposed MPPT.

Working Principle: In the proposed MPPT, the PV array is disconnected from the load for sampling of its open circuit voltage. During the sampling interval the S&H is triggered into the sampling mode [7]. The array voltage is sampled by the S&H and a fraction thereof is kept in the hold capacitor to act as V_{ref} for the converter to latch on to. The sampling time and the sampling period is controlled by a 555 timer and a dual monos table multi vibrator (MMV) [8]. This is shown schematically in Fig. 7.

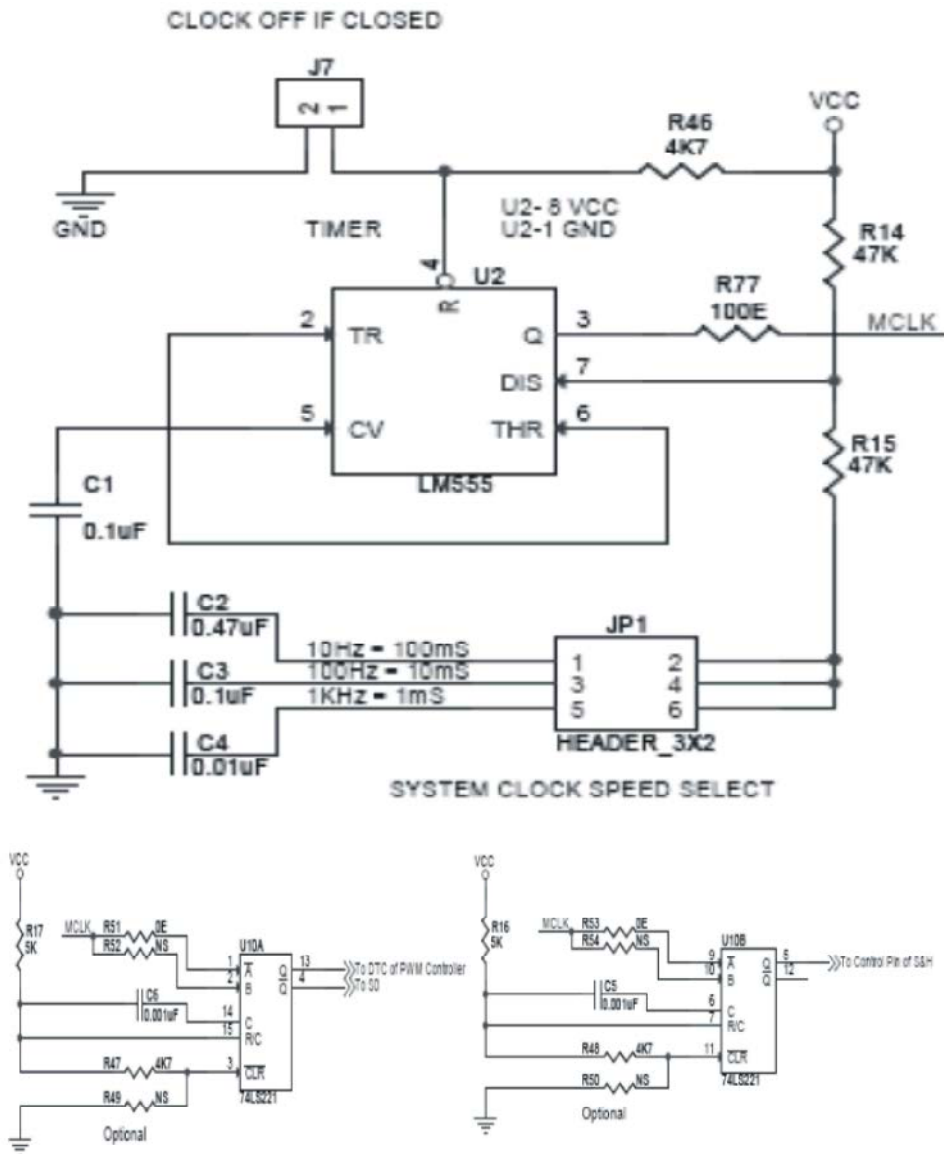


Fig. 8: Circuit diagram of trigger circuit

Both the MMVs are negative edge triggered [12]. The timer produces a falling edge after every 100ms which is the duration of the sampling period. The output pulse width at the true output of the MMV1 is 5 μ s.

As shown in Figure 7, the true output of the MMV1 connected to the dead time control (DTC) of the pulse width modulation (PWM) controller [9], to turn off its output during the sampling interval. The complementary output of MMV1, which is connected to the driving circuit of S0, turns it off and the PV array is disconnected from the load for 5 μ s.

The MMV2 is triggered into the timing state synchronously with MMV1. The output of the MMV2

triggers the S&H into the sampling mode [7]. To ensure that the PV array voltage is sampled well before the array is reconnected to the load and to make allowance for the hold mode [7] settling time of the S&H, the width of the output pulse of the MMV2 is kept shorter than MMV1.

Inference: The proposed circuit was implemented successfully and indoor testing was also performed. A variable DC voltage source was used in series with a variable resistor. Therefore it is evident that the MPPT should always track the input voltage to the converter, such that the input voltage at least receives half of the supply voltage. The voltage factor was accordingly

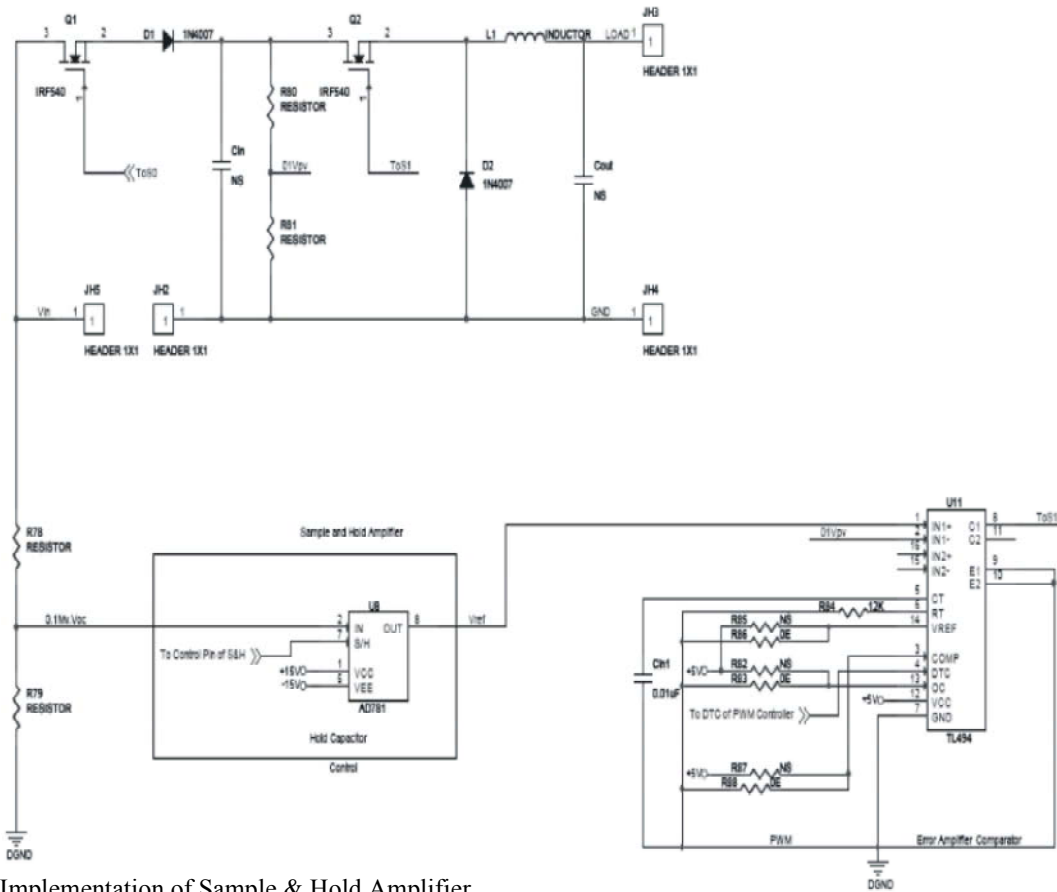


Fig. 9: Implementation of Sample & Hold Amplifier

designed to be at 0.5 and switching frequency at 100 kHz. It is to be noted that the MOSFET is switched off during sampling of the array voltage to produce V_{ref} . After obtaining the corresponding pwm output via the S&H circuit, it is fed to S1, which transfers the PV array voltage to the connected load.

Output Waveforms

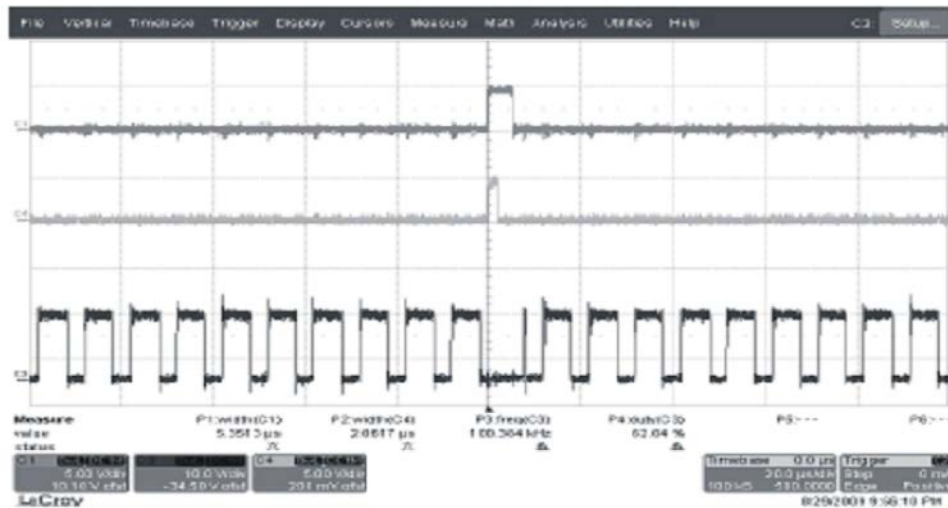


Fig. 10: Waveform visuals of Dual MMVBs & PWM

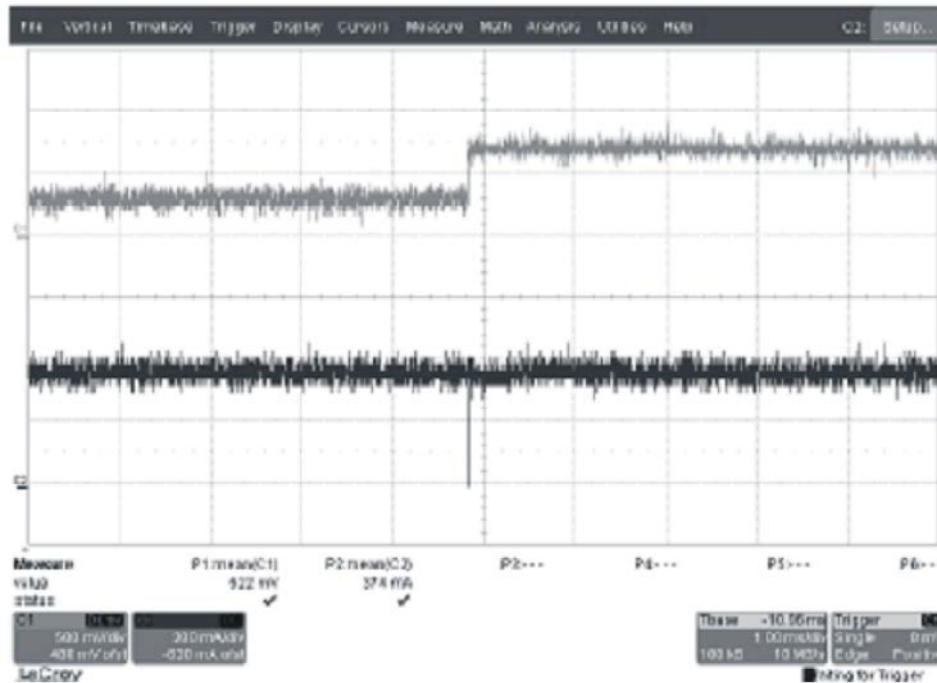


Fig. 11: Sample &Hold Amplifier Outputs

CONCLUSION

The best and simplest maximum power point tracking method was discussed and implemented successfully. Of all the techniques, fractional open circuit voltage based MPPT has proven to be the most economical. A fraction of the PV array is obtained through a sample and hold amplifier, which acts as reference voltage.

The main highlight of the proposed circuit is that it does not involve any controlling device such as a microcontroller or a digital signal processor. Thus, time and again this method proves that this is best opted for low cost and low power electronic applications.

The circuit performs a high-efficiency conversion through an ultra-low-power circuit that requires less than 1 mW. The estimation of the peak power point is done automatically, using a small PV module as reference, whereby sensing operation does not require additional power. Hence, this prototype can be used with any kind of modern embedded systems as a plug-and-play source, avoiding compatibility issues which arise when using other energy sources.

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